

Liquid accelerator

[0001]

The present invention relates to a liquid accelerator. Specifically, the present invention relates to a liquid accelerator which excels in accelerating effect and also excels in storage stability at lower temperatures and inhibitory effect of the alkali-aggregate reaction.

[Background Arts]

[0002]

Conventionally, to prevent the collapses of exposed terrain surfaces such as a face of slope and a tunnel excavation, there have been used spraying processes which spray an accelerated mortar or concrete on the spray surface, in which process an accelerator is added to cement composition such as mortar or concrete. Generally, as the accelerator, alkali metal salts (sodium and potassium) of aluminate, silicic acid, carbonic acid, etc. have been widely used. Since these compounds have strong alkalinity, they have adverse effects on the environment and the human body in spraying operation; for example, they may attack the skin and cause eye inflammation or corneal corrosion thereby impairing visual acuity.

[0003]

Moreover, alkaline accelerators, which contains alkali metals such as sodium or potassium, may pose a risk of inducing alkali-aggregate reaction with the aggregates in concrete and, therefore, are not preferable in the viewpoint of durability of the concrete.

Moreover, sprayed concrete generally includes a large quantity of cement per unit area, and therefore a large quantity of alkali (sodium and potassium) is also induced from the cement. Further, since the ratio of fine aggregates is also large, there was a high probability of causing alkali-aggregate reaction. Thus, when a reactive aggregate was used for sprayed concrete, there was a high risk of causing cracks in the concrete after cure thereby impairing the durability. As the countermeasure of this, attempts have been made to use aggregates which would not contribute to alkali-aggregate reaction or to use low alkali type cement; however, it was difficult to fully prevent the problem.

[0004]

Under these current circumstances, acidic liquid accelerators composed of aluminum sulfate, aluminum hydroxide, and the fluorides of aluminum have been proposed.

For example, a concrete accelerator consisting of aluminum fluoride, acidic or basic solution of aluminum containing aqueous hydrofluoric acid solution of aluminum, lithium silicate, and lithium aluminate has been proposed (see, for example, patent document 1).

Moreover, an accelerator which consists of nitrate, sulfate, glycolate, lactate, etc. of aluminum, a compound forming agent, and a corrosion inhibitor and which contains no alkalis and chlorides has been proposed (see, for example, patent document 2).

Furthermore, an accelerator that contains aluminum salts, which contains aqueous fluorides, and sulfates, and that does not contain alkali metals and chlorides has been proposed (see, for example, document 3). Furthermore, a liquid accelerator containing aluminum, sulfur, sodium, and fluorine has been proposed (see, for example, patent document 4). There has been further proposed an accelerator that consists of a fluoride-containing aqueous aluminum salt, which is obtained through the reaction between the aluminum hydroxides or aluminum oxides and hydrofluoric acid, and a sulfate-containing aqueous aluminum salt such as aluminum sulfate and basic aluminum sulfate, and that does not contain alkali metals and chlorides (see, for example, patent document 5).

[0005]

However, the above described technologies have not provided a liquid accelerator having a sufficient accelerating effect. The present inventors has focused attention on the effects of alkali metals for improving the initial strength development of concrete, and proposed, in Japanese Patent Application No. 2003-62114, a liquid accelerator that contains aluminum sulfate, alkanolamine, alkylene diamine, hydrofluoric acid, and 1 to 8.5% by total alkali of alkali metal salts such as sodium hydroxide, potassium hydroxide, sodium carbonate, potassium carbonate, sodium sulfate, potassium sulfate. However, although this liquid accelerator excelled in accelerating effect and initial strength development, it had a problem in solution stability at low temperatures.

[Patent document 1] Japanese Patent Laid-Open No. 2001-130935.

[Patent document 2] Japanese Patent Laid-Open No. 2001-180994, US 6,514,327

[Patent document 3] Japanese Patent Laid-Open No. 2002-29801.

[Patent document 4] Japanese Patent Laid-Open No. 2002-47048.

[Patent document 5] Japanese Patent Laid-Open No. 2002-80250.

[Disclosure of the Invention]

[Problem to be Solved by the Invention]

[0006]

Accordingly, it is the object of the present invention to provide a liquid accelerator which excels in accelerating effect, and which also excels in storage stability at low temperatures and in inhibitory effect of alkali-aggregate reaction.

[0007]

[Means for Solving the Problem]

The present inventors have eagerly studied to solve the above describe problems eventually finding that all those problems may be solved by using specific lithium salts, and have finally completed the invention.

Thus, the present invention relates to a liquid accelerator composed of a fluoride-containing aqueous aluminum salt, which is obtained through the reaction between aluminum sulfate and hydrofluoric acid, aluminum hydroxide, and one or more kinds of lithium salts selected from the group consisting of lithium hydroxides, lithium carbonates, and lithium sulfates.

The present invention also relates to the above described liquid accelerator in which total alkali content is less than 1 %.

[0008]

Furthermore, the present invention relates to the above described liquid accelerator characterized in that 15 to 35 % by mass of aluminum sulfate, 1 to 5 % by mass of hydrofluoric acid, less than 15 % by mass of aluminum hydroxide, and 3 to 25 % by mass of one or more kinds of lithium salts selected from the group consisting of lithium hydroxides, lithium carbonates, and lithium sulfates are used for the total amount of the liquid accelerator.

[0009]

The present invention further relates to the above described liquid accelerator wherein the ratio A/S of the number of moles of Al_2O_3 (A) to the number of moles of SO_3 (S) in the liquid accelerator is 0.35 to 1.0.

The present invention further relates to the above described liquid accelerator wherein the source of SO_3 is one or more kinds of sulfuric compounds selected from the group consisting of sulfuric acids, aluminum sulfates, lithium sulfates, sodium sulfates, and potassium sulfates.

[0010]

The present invention further relates to the above described liquid accelerator wherein one or more members selected from the group consisting of C_1 to C_{10} organic monocarboxylic and dicarboxylic acids and the metallic salts thereof are contained.

The present invention further relates to the above described liquid accelerator wherein one or more members selected from the group consisting of alkanolamine, alkylene diamine, and triamine are contained.

[0011]

The present invention further relates to the use of the above described liquid accelera-

tor for sprayed mortar or concrete applied to a dry or wet spraying process.

[0012]

The present invention further relates to a process of dry or wet spraying wherein the above described liquid accelerator is added to a cement composition such as mortar or concrete in a transport pipe, a watering nozzle, or a spray nozzle either directly to the mixture by means of an accelerator feed device, or to the water content.

[0013]

The present invention further relates to a process of dry or wet spraying characterized in that the above described liquid accelerator is added to base mortar or concrete which is added with a high-range AE water-reducing agent and/or a retarder of polycarbonic acid base and which is applied to the spraying process.

[Advantages of the Invention]

[0014]

The liquid accelerator of the present invention enables to reduce the total alkali of the accelerator by using specific lithium salts and eliminates crystalline precipitation at low temperatures thereby providing excellent storage stability at low temperatures.

By enabling the reduction of the total alkali as describe above, the invention reduces the effect on the environment and human body during spraying operation and the like, and provides the inhibitory effect on the alkali-aggregate reaction.

[0015]

Since the accelerator of the present invention utilizes a fluoride-containing aqueous aluminum salt containing hydrofluoric acid, the accelerator provides a good spraying workability without raising the initial accelerating effect too high, thereby making it possible to prevent the exfoliation of concrete during concrete spraying and enable a thick deposit of concrete.

Moreover, since the above described fluoride-containing aqueous aluminum salt is obtained by adding hydrofluoric acid to aluminum sulfate, the manufacturing of the accelerator poses low risk and safer than conventional ones.

[The Best Mode for Carrying out the Invention]

[0016]

Hereinafter, the present invention will be described in more detail.

The present invention is a liquid accelerator composed of a fluoride-containing aqueous aluminum salt, which is obtained through the reaction between aluminum sulfate and hydrofluoric acid, aluminum hydroxide, and one or more lithium salts selected from the group

consisting of lithium hydroxides, lithium carbonates, and lithium sulfates, with the total alkali being less than 1 %, and preferably not more than 0.5%. The term "total alkali (%)" in the present invention is expressed by the equation: $\text{Na}_2\text{Oeq} = \text{sodium oxide (Na}_2\text{O)} + 0.658 \text{ potassium oxide (K}_2\text{O)}$. When the total alkali in the liquid accelerator exceeds 1%, the stability at low temperatures degrades resulting in crystal precipitation, which is not preferable, and also the alkali-aggregate reaction will be negatively affected.

[0017]

The aluminum sulfate to be used in the present invention may be aluminum sulfate which is generally used as accelerating agent, and it may be either fully or partly hydrated. A typical grade is 17% aluminum sulfate ($\text{Al}_2(\text{SO}_4)_3 \cdot 14.3\text{H}_2\text{O}$) (the name is after the content of aluminum oxides) and, when using a different grade, a proper quantity may be calculated based on this grade. Also, it is preferably composed that the content of aluminum sulfate is, as the amount of $\text{Al}_2(\text{SO}_4)_3$, 15 to 35 % by mass of the total liquid accelerator.

[0018]

The hydrofluoric acid to be used in the present invention is generally used as a HF aqueous solution of about 40 to 55 % by mass. And the proportion of hydrofluoric acid (as HF) subjected to the reaction with aluminum sulfate is preferably 1 to 5 % by mass of the total liquid accelerator.

[0019]

The present invention utilizes a fluoride-containing aqueous aluminum salt which is obtained by the reaction between aluminum sulfate and hydrofluoric acid; it is preferable that aluminum sulfate of 15 to 35 % by mass is reacted with hydrofluoric acid of 1 to 5 % by mass, which would provide a good solution stability at low temperatures for a long term.

Since the above described fluoride-containing aqueous aluminum salt is obtained by adding hydrofluoric acid to aluminum sulfate unlike a conventional manner in which aluminum compounds are added to hydrofluoric solution, its manufacturing poses low risk and is safer.

[0020]

The aluminum hydroxide to be used in the present invention may be amorphous aluminum oxide which is commonly used as accelerating agent, and which is preferably contained up to 15 % by mass of the liquid accelerator. It is also possible to use inexpensive crystalline aluminum hydroxides; however, those have a low solubility thereby leading to a decline of solution stability at low temperatures, and therefore can not provide the same level performance as that of the amorphous type.

[0021]

The lithium salt to be used in the present invention may be any of lithium hydroxide, lithium carbonate, and lithium sulfate, or may be combinations of one or more of them. The preferable proportion of the lithium salt is 3 to 25 % by mass of the total liquid accelerator.

The content of the lithium ion in the liquid accelerator is preferably such that the molar ratio Li/Na is not less than 0.6 for the Na_2O equivalent introduced from the mortar or concrete to inhibit alkali-aggregate reaction. Moreover, in the practical use of the liquid accelerator, the content of the lithium ion in the liquid accelerator is preferably in the range of 0.01 to 1.0 % by the mass of the cement in the mortar or concrete.

[0022]

The liquid accelerator of the present invention has a ratio A/S: the number of moles of Al_2O_3 (A) to the number of moles of SO_3 (S), of 0.35 to 1.0. The range is preferably 0.35 to 0.55, and when A/S is within this range, the liquid accelerator exerts an excellent initial strength development. Moreover, the liquid accelerator of the present invention may utilize sulfuric compounds such as sulfuric acid, aluminum sulfate, lithium sulfate, sodium sulfate, and potassium sulfate as the source of SO_3 for controlling A/S. In the case of sodium sulfate and potassium sulfate, they may be used by an amount that total alkali is less than 1 %. The preferable proportion of the sulfuric compounds is 5 to 35 % by mass of the total liquid accelerator.

[0023]

The liquid accelerator of the present invention may contain C_1 to C_{10} organic mono- and di-carboxylic acids and one or more metal salts thereof for the purpose of improving the initial strength of concrete. The C_1 to C_{10} organic mono- and di-carboxylic acids and metal salts thereof may be preferably formic acid, oxalic acid, and glycol acid as well as the metal salts thereof, and other acids such as acetic acid, propionic acid, succinic acid, citric acid and tartaric acid may also be used. Moreover, the proportions of these components are preferably 1 to 10 % by mass, and more preferably 4 to 8 % by mass of the total liquid accelerator

[0024]

Furthermore, to improve the solution stability, the liquid accelerator of the present invention may be combinations of one or more members of alkanolamine, alkylene diamine, and alkylene triamine. The components of these are preferably ethylenediamine, ethylenetriamine, diethanolamine or triethanolamine, and more preferably diethanolamine. These components are in the proportion of preferably 0.1 to 10 % by mass, and more preferably 0.1 to 8 % by mass of the total liquid accelerator.

[0025]

The liquid accelerator of the present invention can be prepared in a simple manner by mixing the above explained components in any order and stirring the mixture, final mixture having a pH of 2 to 8 and containing water of 40 to 70 % by mass.

[0026]

The suitable use of the liquid accelerator of the present invention is to add the liquid accelerator of the present invention into a cement composition such as mortar or concrete applied to conventional dry or wet spraying process. In using it, the liquid accelerator of the present invention may be added by the amount of 5 to 12 % by mass with respect to the mass of the cement in the cement composition, although this will vary depending on the applications.

[0027]

The present invention is a process of dry or wet spraying wherein the above described liquid accelerator is added to a cement composition such as mortar or concrete in a transfer pipe, watering nozzle, or a spraying nozzle either directly to the mixture by means of an accelerator feed device, or to the water content.

[0028]

Moreover, the present invention is a process of spraying wherein the liquid accelerator is added by a method shown in [0027] to a base mortar or concrete which is added with high-range AE water-reducing agent and/or a retarder of polycarboxylic acid base and which is applied to the spraying process.

The high-range AE water-reducing agent of polycarboxylic acid base of the present invention may be any commercially available one for general purpose uses. Commercially available high-range AE water-reducing agents of polycarboxylic acid base includes: polycarboxylic acid base cement water-reducing agent having polyalkyleneoxide group such as JP,A,58-38380 (copolymer of polyethylene glycol methacrylate and methacrylic acid), JP,A,62-70250 (copolymer of polyethylene glycol methacrylate, methacrylic acid, and amide compound adduct having polyalkyleneoxide of unsaturated carboxylic acid); and ones containing JP,A,05-213644 (copolymer of polyethylene glycol methacrylate and methacrylic acid), JP,A,05-238795 (copolymer selected from polyalkylene glycol diester base monomers having unsaturated bonds, acrylic acid base monomers and polyalkylene glycol monoester monomers having unsaturated bond) JP,A,09-286645 (copolymer of polyethylene glycol methacrylate, of which oxyethylene group has different chain lengths of 1 to 10 and 11 to 100, and methacrylic acid), Japanese Patent No.2541218 (copolymer of polyoxyalkylene de-

rivatives and maleic anhydride) JP,A,07-215746 (copolymer of polyoxyalkylene derivatives and maleic anhydride), JP,A,05-310458 (copolymer of alkenyl ether and maleic anhydride), JP,A,04-74748 (copolymer of olefins of carbon number 2 to 8 and ethylene-base unsaturated dicarboxylic anhydride), JP,A,62-83344 (metallic complex with polyacrylic acid or copolymers of olefins of carbon number 2 to 8 and ethylene-base unsaturated dicarboxylic acid etc.), JP,A,2001-180998 (concrete admixture which contains copolymer mixture which is obtained by copolymerizing a specific monomer (A) such as ethylene-base unsaturated carboxylic derivatives having polyoxyalkylene group, and another specific monomer (B) such as (meth)acrylic acid, and in which the molar ratio (A)/(B) is changed at least once during the reaction), JP,B,06-99169 (polyethylene-imine compound consisting of poly(acidic group substituted alkyl group and/or acidic group substituted acyl group)polyethylene-imine and poly(acidic group substituted alkyl group and carbamoyl alkyl group)polyethylene-imine), JP,A,08-283350 (oxyalkyleneglycol-alkenyl ether and unsaturated dicarboxylic acid derivatives and vinyl-base polyalkyleneglycol compounds, polysiloxane compounds or ester compounds), JP,A,2000-351820 (copolymer based on unsaturated monocarboxylic derivatives or dicarboxylic derivatives and oxyalkyleneglycol-alkenyl ether group).

[0029]

The retarder in the present invention may be exemplified by phosphonic acid derivatives selected from the group consisting of aminotri(methylenephosphonic acid), aminotri(methylenephosphonic acid) 5 sodium salt, 1-hydroxyethylidene-1,1-diphosphonic acid, 1-hydroxyethylidene-1,1-diphosphonic acid 4 sodium salt, ethylenediaminetetra(methylenephosphonic acid), ethylenediaminetetra(methylenephosphonic acid) calcium/sodium salt, hexamethylene-diaminetetra(methylenephosphonic acid), hexamethylene-diaminetetra(methylenephosphonic acid) potassium salt, diethylenetriamine-penta(methylenephosphonic acid), and diethylenetriaminepenta(methylenephosphonic acid) sodium salt; and hydroxycarbonic acid and the salts thereof selected from salicylic acid, citric acid, lactic acid, gluconic acid, tartaric acid, muconic acid, and glucoheptanoic acid. Preferable retarder may be exemplified by ones containing phosphonic acid derivatives and citric acid and/or gluconic acid, and the salts thereof.

[Examples]

[0030]

Hereinafter, the present invention will be explained in detail referring to experimental examples 1 to 4. The materials, and the composition and measurement method of the mortar

used for the experiments are shown below.

1. Materials used and mortar composition

#Cement: Ordinary portland cement manufactured by TAIHEIYO CEMENT Co.

total alkali: 0.58%

#Fine aggregate: OI River System pit sand

Reactive aggregate

#High-range AE water-reducing agent: Nt-1000 (Manufactured by NMB Co., Ltd.)

#Retarder: DELVOCRETE (Manufactured by NMB Co., Ltd.)

#Conventional sample 1: See Table 2, 10 % by weight for the cement mass

#Conventional sample 2: Potassium aluminate, 10% by weight for the cement

mass.

#Invention samples 1 to 9: 10 % by weight for the cement mass.

#Mortar composition: water/cement ratio (W/C) = 40 %, sand/cement ratio (S/C) = 2.1

#Measurement method

Starting time: Time needed for the Proctor penetration resistance value to reach 3.5 N/mm²

Compressive strength: In accordance with JIS R 5201

Change rate of length: In accordance with JIS A 1804

[0031]

(Experimental example 1)

The results of the mortar test are shown in Table 1 and Figure 1 for the cases in which the A/S ratio of the liquid accelerator is varied from 0.35 to 1.27. As seen in Table 1 and Figure 1, when the A/S of the liquid accelerator is within the range of 0.35 to 1.27, a sufficient initial strength was developed at the ages of 3 and 24 hours.

[0032]

[Table 1]

| Accelerator type | A/S | Al ₂ O ₃ | SO ₄ ²⁻ | Compressive strength (N/mm ²) | |
|-------------------|------|--------------------------------|-------------------------------|---|----------|
| | | | | 3 hours | 24 hours |
| Invention sample1 | 0.35 | 8.50 | 22.9 | 1.05 | 15.4 |
| Invention sample2 | 0.44 | 9.03 | 19.5 | 1.43 | 15.8 |
| Invention sample3 | 0.48 | 9.25 | 18.3 | 1.55 | 13.8 |
| Invention sample4 | 0.50 | 9.4 | 17.8 | 1.65 | 13.5 |
| Invention sample5 | 0.54 | 9.6 | 16.8 | 1.71 | 13.0 |
| Invention sample6 | 0.69 | 10.3 | 14.1 | 1.35 | 8.94 |
| Invention sample7 | 0.93 | 11.8 | 12.0 | 1.18 | 6.25 |
| Invention sample8 | 1.27 | 12.8 | 9.58 | 0.93 | 5.78 |

[0033]

(Experimental example 2)

The solution stability at low temperatures were compared using the conventional sample 1 and the invention sample 9 shown in Table 2. Table 3 shows the result of the tests in which the liquid accelerators were stored at temperatures of -5, 5, 10, 20, 30, 40 degrees C. for three months. The invention sample 9 showed a good solution stability without crystal precipitation even at low temperatures for a long period.

[0034]

[Table 2]

| Component | Component sample 1 (% by mass) | Invention sample 9 (% by weight) |
|---|-----------------------------------|-------------------------------------|
| Al ₂ (SO ₄) ₃ | 18 | 25 |
| Al(OH) ₃ | 5 | 2 |
| HF | 2 | 2 |
| (COOH) ₂ | 5 | 5 |
| DEA | 2 | 2 |
| Na ₂ SO ₄ | 10 | - |
| Li ₂ CO ₃ | - | 5 |

[0035]

[Table 3]

| Accelerator type | Ambient temperature | | | | | |
|----------------------|---------------------|-----|------|------|------|------|
| | -5°C | 5°C | 10°C | 20°C | 30°C | 40°C |
| Conventional sample1 | × | × | ○ | ○ | ○ | ○ |
| Invention sample | ○ | ○ | ○ | ○ | ○ | ○ |

Evaluation method: 'circle' indicates 'good', 'x' indicates 'crystal precipitation'

[0036]

(Experimental example 3)

Using the conventional sample 1 and the invention sample 9 shown in Table 2, the starting time and the development of the compressive strength were compared by the mortar test. As seen from the mortar test results shown in Table 4, the invention sample 9 showed an earlier starting time than the conventional sample 1 and also showed a good initial strength development characteristics. Further, when the invention sample 9 and the retarder were used together, the starting time was earlier and also the initial strength development was good.

[0037]

[Table 4]

| Accelerator type | Starting time (minute-second) | Compressive strength (N/mm ²) | | | |
|-------------------------------|----------------------------------|---|----------|--------|---------|
| | | 6 hours | 24 hours | 7 days | 28 days |
| Conventional sample 1 | 9-00 | 4.68 | 18.8 | 52.5 | 63.1 |
| Invention sample 9 | 4-00 | 4.62 | 18.5 | 52.4 | 64.1 |
| Invention sample 9 + retarder | 9-00 | 4.88 | 19.2 | 53.3 | 63.8 |

[0038]

(Experimental example 4)

Using the conventional sample 2 shown in Table 2, a test was conducted in accordance with JISA1804 Concrete Production Process Management Test Method: "Alkali-silica reactivity test of aggregate (Rapid determination)." The solution was adjusted by using NaOH aqueous solution so that total Na₂O equivalent quantity contained in the mortar is 0.8%, 1.0%. As shown in Table 5, the invention sample 9 showed an inhibitory effect on the alkali-aggregate reaction.

[0039]

[Table 5]

| Accelerator type | Change rate of length | |
|-----------------------|---|---|
| | Equivalent Na ₂ O from cement = 0.8% | Equivalent Na ₂ O from cement = 1.0% |
| Conventional sample 2 | 0.25 | 0.36 |
| Invention sample 9 | 0.03 | 0.05 |

[0040]

(Experimental example 5)

Using the concrete composition shown in Table 6, and the accelerators shown in Table 7, a thick deposit capability test of sprayed concrete was conducted. Concrete spraying was conducted on the top end of a tunnel until an exfoliation occurred and the average thickness of the sprayed concrete was measured. As shown in Table 7, by adding HF there was observed an effect of increasing the deposit thickness of sprayed concrete.

[Table 6]

| W/C | s/a | Unit quantity (kg/m ³) | | | |
|------|-----|------------------------------------|-----|-----|-----|
| | | W | C | S | G |
| 42.2 | 60 | 190 | 450 | 991 | 678 |

[Table 7]

| Accelerator type | Mass of HF (%) | Top end (thick deposit capability) |
|------------------|----------------|------------------------------------|
| | | Average sprayed thickness (cm) |
| Accelerator 1 | 0 | 23 |
| Accelerator 2 | 2 | 35 |
| Accelerator 3 | 4 | 37 |

[Industrial Applicability]

[0041]

According to the present invention, there is provided a liquid accelerator which excels in accelerating effect and which also excels in the storage stability at low temperatures and the

inhibitory effect of the alkali-aggregate reaction.

[Brief Description of Drawing]

[0042]

[Figure 1] Fig.1 shows the results of initial strength for the cases in which the A/S ratio is varied.